NOISE CONTROL FOR A BETTER ENVIRONMENT

# Method to calculate $L_{\text {AFmax }}$ noise map from $L_{\text {Aeq }}$ noise maps, for roads and railways 

Rosão, Vitor ${ }^{1}$

Aguileira, Ana ${ }^{2}$
SCHIU, Vibration and Noise Engineering
Av. Villae de Milreu, Bloco E, Loja E, Estoi
8005-466 Faro
Portugal


#### Abstract

This paper presents the simple theoretical relations between $\boldsymbol{L}_{A F m a x}$ and $\boldsymbol{L}_{\text {Aeq }}$, for roads (simulation each vehicle as a moving point source) and railways (simulation of each vehicle/train as a moving line source with length $l$ ). From these relations more valid for close proximity to the source - and knowing the typical values of $\boldsymbol{L}_{\text {Aeq }}$ for roads and railways, according with the standard methods available, the associated calculation of typical values of $L_{\text {AFmax }}$ was performed. Knowing - by this way or another - the $L_{A F m A x}$ close to the roads or railways, the typical noise source, on typical software, must be divided into small parts, with 1 m length each. After that, one of these small parts must be converted on a line source with a sound power that give, 1 m distance, an $L_{A e q}$ equal to the $L_{A F M a x}$ we want (the spectrum must be adjusted accordingly). All the other small parts, related, must be converted on a line source with the same sound power level. An independent noise map must be calculated for each small line source. For each noise receiver the $\boldsymbol{L}_{\text {AFmax }}$, from a passby, is the greater value of all line source independent noise maps. This procedure can consume too much time, depending on the number of small line sources we have. Fortunately, some available software - for example the Cadna A - permits the calculation of $\boldsymbol{L}_{\text {AFmax }}$ noise maps from different line sources. To do that, Cadna A needs the introduction of the difference value between $L_{\text {AFMax }}$ and $L_{\text {Aeq }}$ for each small line source, so that must be calculated. At major distances to the road or railway, this $\boldsymbol{L}_{\text {AFMax }}$ noise map gives smaller values than the regular $\boldsymbol{L}_{\text {Aeq }}$ noise map, so, by definition, the global $L_{\text {AFMax }}$ noise map must have the greater value, in each receiver point, from these two noise maps.


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## 1. INTRODUCTION

The great majority of the commercial software to produce outside noise environmental maps, can just produce, typically for roads and railways, $L_{\text {Aeq }}$ noise maps, not $L_{\text {AFmax }}$ noise maps (definitions of $L_{\text {Aeq }}$ and $L_{\text {AFmax }}$ in ISO 1996-1 [1]). The main reason is the fact that the standard methods used were developed for $L_{\text {Aeq }}$ values not for $L_{A F m a x}$ values.

In some cases can be important to know not just the $L_{\text {Aeq }}$ values but also the $L_{\text {AFmax }}$ values.

This paper attempts to define a way to obtain $L_{\text {AFmax }}$ values based on $L_{\text {Aeq }}$ values.

## 2. THEORETICAL RELATIONS

For a passing light car, or for a passing truck, at constant speed $v[\mathrm{~m} / \mathrm{s}]$, we can simulate this situation as a point source, with a specific Noise Power Level $L_{A w}$, and the instantaneous Noise Levels $L_{\text {Aeq }}(t)$ ( $t$ in seconds), on a receiver point at a perpendicular distance $d_{\perp}[\mathrm{m}]$, can be written, by simplicity and applicability, as (Annex A1.1 of [2] or [3]):

$$
\begin{equation*}
L_{A e q}(t)=L_{A w}-11-20 \log \left(\sqrt{\left(d_{\perp}\right)^{2}+(v t)^{2}}\right) \tag{1}
\end{equation*}
$$

The $L_{\text {AFmax }}$ of this variation occurs at $t=0$ (the equation (1) is written in a way that the time before the pass-by is negative and the time after positive):

$$
\begin{equation*}
L_{A F \max }=L_{A w}-11-20 \log \left(d_{\perp}\right) \tag{2}
\end{equation*}
$$

The integration of $L_{\text {Aeq }}(t)$ during the pass-by can be written as $L_{A e q, T}$ (where $T$ is the duration of the pass-by). For a typical time of $1 \mathrm{~h}(1 / 2$ hour before and $1 / 2$ hour after the pass-by) the relation of $L_{\text {Aeq, 1h }}$ with $L_{A F m a x}$ can be written as (Annex A1.1 of [2]):

$$
\begin{equation*}
L_{\text {Aeq, } 1 \mathrm{~h}} \approx L_{A F m a x}-25+10 \log \left(d_{\perp}\right)-10 \log \left(v_{\mathrm{km} / \mathrm{h}}\right) \tag{3}
\end{equation*}
$$

or:

$$
\begin{equation*}
L_{A F \max } \approx L_{A e q, 1 \mathrm{~h}}+25-10 \log \left(d_{\perp}\right)+10 \log \left(v_{\mathrm{km} / \mathrm{h}}\right) \tag{4}
\end{equation*}
$$

where $v_{\mathrm{km} / \mathrm{h}}$ is the speed of the car, or of the truck, in $\mathrm{km} / \mathrm{h}$.
For a train, with length $l[\mathrm{~m}]$, the previous point source approximation cannot be used anymore. Using now a linear source of length $l$ the equations (3) and (4) can be rewritten as (Annex A1.2 of [2]), taking into account $L_{A E}=L_{\text {Aeq }}+10 \log (T)$ ):

$$
\begin{align*}
& L_{\text {Aeq }, 1 \mathrm{~h}} \approx L_{\text {AFmax }}-28-10 \log \left(\operatorname{tg}^{-1}\left(\frac{l}{2 d_{\perp}}\right)\right)+10 \log \left(\left(\frac{l}{v \mathrm{~km} / \mathrm{h}}\right)\right)  \tag{5}\\
& L_{\text {AFmax }} \approx L_{\text {Aeq }, 1 \mathrm{~h}}+28+10 \log \left(\operatorname{tg}^{-1}\left(\frac{l}{2 d_{\perp}}\right)\right)-10 \log \left(\left(\frac{l}{v \mathrm{~km} / \mathrm{h}}\right)\right) \tag{6}
\end{align*}
$$

The equations (4) and (6) are the main equations for obtain $L_{A F m a x}$ when we know the $L_{A e q}$ of a pass-by car, truck or train.

Since the global $L_{\text {Aeq,global }}$ of a road or a railway depends also on the number $n$ of vehicles passing by, this value can be written as:

$$
\begin{equation*}
L_{\text {Aeq,global }}=L_{\text {Aeq, } 1 \text { vehicle }}+10 \log (n) \tag{7}
\end{equation*}
$$

Once the $L_{A F m a x, 1 \text { vehicke }}$ of 1 vehicle do not depends on the quantity of vehicles, there is a quantity $n$, for a given distance $d_{\perp}$ to the road or railway, and for a given speed $v_{\mathrm{km} / \mathrm{h}}$ of the vehicles, where $L_{\text {Aeq,global }}$ is equal to $L_{A F m a x, \text {, vehicle. }}$. Above this quantity $L_{\text {Aeq,global }}$ is higher than $L_{A F m a x, ~ 1 v e h i c l e ~}$ and, by definition, $L_{A F m a x, \text { global }}$ becomes equal to $L_{\text {Aeq,global }}$.

In Table 1 (roads) and Table 2 (railways) is showed the values of $L_{A F m a x}-L_{\text {Aeq, } 1 \text { h }}$, according to equations (4) and (6), for different values of $d_{\perp}$ and $v_{\mathrm{km} / \mathrm{h}}$. For railways is assumed, by simplicity and applicability, $l=50 \mathrm{~m}$.

In Table 3 (roads) and Table 4 (railways) is showed the values of $n$ that makes $10 \log (n)$ equal to, respectively, the values of Table 1 and 2 . So, above this quantity - for the associated $d_{\perp}$ and $v_{\mathrm{km} / \mathrm{h}}$ values $-L_{A F m a r, g l o b a l}$ becomes equal to $L_{A e q, \text { global }}$.

Of course, these relations assume that the equations (4) and (6) are valid for all the distances, but in reality, for bigger distances, there are, normally, other kind of sound attenuations, like atmospheric, ground and obstacles attenuations, that makes the equations (4) and (6) not anymore right valid, so the relations presented are just indicative.

The equations (4) and (6) are just valid fore close distances to the road or railway.
For the NMPB'96 (the interim European noise method for roads [4]), SRMII (the interim noise method for railways [4]) and for CNOSSOS (the new harmonized European method for road, railways and other noise sources [5]) we have calculated the $L_{A e q}$ value of one pass-by, and we have obtained the values showed on Table 5 (roads) and Table 6 (railways). For Railways we just used the SRM II, because, so far, just for these we have, in Portugal, relations between the Standard Trains and the Portuguese reality [6].

Table 1: Differences between $L_{\text {AFmax, Ivehicle }}$ and $L_{\text {Aeq,lvenicle }}$ (roads)

| $\begin{aligned} & \text { Distances } d_{\perp} \\ & {[\mathrm{m}]} \end{aligned}$ | $L_{\text {AFmax, }}$ 1vehicle $-L_{\text {Aeq, }}$,vehicle $[$ [equation (4)] [dB(A)] |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Speed |  |  |  |  |
|  | $30 \mathrm{~km} / \mathrm{h}$ | $50 \mathrm{~km} / \mathrm{h}$ | $70 \mathrm{~km} / \mathrm{h}$ | $90 \mathrm{~km} / \mathrm{h}$ | $120 \mathrm{~km} / \mathrm{h}$ |
| 1 | 40 | 42 | 43 | 45 | 46 |
| 7.5 | 31 | 33 | 35 | 36 | 37 |
| 15 | 28 | 30 | 32 | 33 | 34 |
| 30 | 25 | 27 | 29 | 30 | 31 |
| 60 | 22 | 24 | 26 | 27 | 28 |
| 120 | 19 | 21 | 23 | 24 | 25 |
| 240 | 16 | 18 | 20 | 21 | 22 |
| 480 | 13 | 15 | 17 | 18 | 19 |

Table 2: Differences between $L_{A F m a x, \text {,lvehicle }}$ and $L_{\text {Aeq, ivehicle }}$ (railways)

| Distances $\boldsymbol{d}_{\perp}$ <br> $[\mathbf{m}]$ | $\boldsymbol{L}_{\text {AFmax, }}$ vehicle $-\boldsymbol{L}_{\text {Aeq, } 1 \text { vehicle }}$ [equation (6); $\left.\boldsymbol{l}=\mathbf{5 0} \mathbf{~ m}\right][\mathrm{dB}(\mathbf{A})]$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{3 0} \mathbf{~ k m} / \mathbf{h}$ | $\mathbf{5 0} \mathbf{~ k m} / \mathbf{h}$ | $\mathbf{7 0} \mathbf{~ k m} / \mathbf{h}$ | $\mathbf{9 0} \mathbf{~ k m} / \mathbf{h}$ | $\mathbf{1 2 0} \mathbf{~ k m} / \mathbf{h}$ |
| 1 | 28 | 30 | 31 | 32 | 34 |
| 7.5 | 27 | 29 | 31 | 32 | 33 |
| 15 | 26 | 28 | 30 | 31 | 32 |
| 30 | 24 | 26 | 28 | 29 | 30 |
| 60 | 22 | 24 | 25 | 27 | 28 |
| 120 | 19 | 21 | 23 | 24 | 25 |
| 240 | 16 | 18 | 20 | 21 | 22 |
| 480 | 13 | 15 | 17 | 18 | 19 |

Table 3: Values of $n$ that make $10 \log (n)$ equal to the value of Table 1 (roads)

| Distances $\boldsymbol{d}_{\perp}$ <br> $[\mathbf{m}]$ | Values of $\boldsymbol{n} / \mathbf{h o u r}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{3 0} \mathbf{~ k m} / \mathbf{h}$ | $\mathbf{5 0} \mathbf{~ k m} / \mathbf{h}$ | $\mathbf{7 0} \mathbf{~ k m} / \mathbf{h}$ | $\mathbf{9 0} \mathbf{~ k m} / \mathbf{h}$ | $\mathbf{1 2 0} \mathbf{~ k m} / \mathbf{h}$ |
| 1 | 10000 | 15849 | 19953 | 31623 | 39811 |
| 7.5 | 1259 | 1995 | 3162 | 3981 | 5012 |
| 15 | 631 | 1000 | 1585 | 1995 | 2512 |
| 30 | 316 | 501 | 794 | 1000 | 1259 |
| 60 | 158 | 251 | 398 | 501 | 631 |
| 120 | 79 | 126 | 200 | 251 | 316 |
| 240 | 40 | 63 | 100 | 126 | 158 |
| 480 | 20 | 32 | 50 | 63 | 79 |

Table 4: Values of $n$ that make 10log(n) equal to the value of Table 2 (railways)

| Distances $\boldsymbol{d}_{\perp}$ <br> $[\mathbf{m}]$ | Speed |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{3 0} \mathbf{~ k m} / \mathbf{h}$ | $\mathbf{5 0} \mathbf{~ k m} / \mathbf{h}$ | $\mathbf{7 0} \mathbf{~ k m} / \mathbf{h}$ | $\mathbf{9 0} \mathbf{~ k m} / \mathbf{h}$ | $\mathbf{1 2 0} \mathbf{~ k m} / \mathbf{h}$ |
| 1 | 631 | 1000 | 1259 | 1585 | 2512 |
| 7.5 | 501 | 794 | 1259 | 1585 | 1995 |
| 15 | 398 | 631 | 1000 | 1259 | 1585 |
| 30 | 251 | 398 | 631 | 794 | 1000 |
| 60 | 158 | 251 | 316 | 501 | 631 |
| 120 | 79 | 126 | 200 | 251 | 316 |
| 240 | 40 | 63 | 100 | 126 | 158 |
| 480 | 20 | 32 | 50 | 63 | 79 |

Table 5: $L_{\text {Aeq }}$ values (roads)

| Vehicle | Distance to the road [m] | $L_{\text {Aeq }}$ values at 1 and 7.5 m distance from road (pass-by off one vehicle/hour) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $30 \mathrm{~km} / \mathrm{h}$ | $50 \mathrm{~km} / \mathrm{h}$ | $\begin{array}{r} \text { Speed } \\ 80 \mathrm{~km} / \mathrm{h} \end{array}$ | $100 \mathrm{~km} / \mathrm{h}$ | $120 \mathrm{~km} / \mathrm{h}$ |
| NMPB'96 |  |  |  |  |  |  |
| Light | 1 | 45 | 46 | 51 | 53 | 54 |
| Light | 7.5 | 38 | 39 | 43 | 45 | 47 |
| Trucks | 1 | 61 | 58 | 59 | 61 | 61 |
| Trucks | 7.5 | 53 | 51 | 52 | 54 | 54 |
| CNOSSOS |  |  |  |  |  |  |
| Light | 1 | 40 | 43 | 48 | 50 | 52 |
| Light | 7.5 | 34 | 37 | 41 | 44 | 46 |
| Trucks (Cat.2) | 1 | 49 | 49 | 51 | 52 | 54 |
| Trucks <br> (Cat.2) | 7.5 | 42 | 43 | 45 | 46 | 47 |
| Trucks (Cat.3) | 1 | 52 | 52 | 54 | 55 | 56 |
| Trucks <br> (Cat.3) | 7.5 | 45 | 46 | 47 | 49 | 50 |

Table 6: $L_{\text {Aeq }}$ values for SRMII categories (railways)

| Train | Distance to the railway [m] | $L_{A e q}$ values at 1 and 7.5 m distance from railway (pass-by off one vehicle/hour) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $30 \mathrm{~km} / \mathrm{h}$ | $50 \mathrm{~km} / \mathrm{h}$ | $\begin{gathered} \text { Speed } \\ 80 \mathrm{~km} / \mathrm{h} \end{gathered}$ | $100 \mathrm{~km} / \mathrm{h}$ | $120 \mathrm{~km} / \mathrm{h}$ |
| SRMII |  |  |  |  |  |  |
| C02 | 1 | 54 | 56 | 59 | 61 | 63 |
| C02 | 7.5 | 49 | 51 | 54 | 56 | 58 |
| C03 | 1 | 48 | 50 | 53 | 55 | 56 |
| C03 | 7.5 | 43 | 45 | 48 | 50 | 51 |
| C03m | 1 | 51 | 53 | 56 | 58 | 60 |
| C 03 m | 7.5 | 45 | 47 | 51 | 52 | 54 |
| C05d | 1 | 61 | 60 | 61 | 61 | 62 |
| C05d | 7.5 | 55 | 54 | 55 | 56 | 57 |
| C08 | 1 | 51 | 53 | 55 | 56 | 58 |
| C08 | 7.5 | 45 | 47 | 50 | 51 | 52 |
| C09c | 1 | 50 | 54 | 57 | 59 | 60 |
| C09c | 7.5 | 44 | 48 | 51 | 53 | 54 |

In Table 7 we have the $L_{\text {Aeq }}$ values of the Portuguese Trains, taking into account its relationship with SRM II categories, according [6].

With the equations (4) and (6) we did the calculation of the associated values of $L_{A F m a x}$, from the $L_{A e q}$ values, as presented in Table 8 and Table 9. So, these are the $L_{A F m a x}$ values that, theoretically, we can expect near to a road or a railway.

Table 7: $L_{\text {Aeq }}$ values for Portuguese Trains [6]

| Train | Relation <br> to SRMI <br> Category | Length [m] | Distance to the railway [m] | $L_{A e q}$ values at 1 and 7.5 m distance from railway (pass-by off one vehicle/hour) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Speed [km/h] |  |  |  |  |
|  |  |  |  | 30 | 50 | 80 | 100 | 120 |
| SRMII - Portuguese Trains |  |  |  |  |  |  |  |  |
| UQE 3150/3250 | $4.6 \times \mathrm{C} 02$ | 79 | 1 | 61 | 63 | 66 | 68 | 70 |
| UQE 3150/3250 | $4.6 \times \mathrm{C} 02$ | 79 | 7.5 | 56 | 58 | 61 | 63 | 65 |
| $\begin{gathered} \text { UQE 2X00+ } \\ \text { UQE2X00 } \\ \hline \end{gathered}$ | $25 \times \mathrm{C} 02$ | 192 | 1 | 68 | 70 | 73 | 75 | 77 |
| $\begin{aligned} & \text { UQE } 2 \mathrm{X} 00+ \\ & \text { UOE2X00 } \end{aligned}$ | $25 \times \mathrm{C} 02$ | 192 | 7.5 | 63 | 65 | 68 | 70 | 72 |
| UQE 3500 | $14.6 \times \mathrm{C} 08$ | 107 | 1 | 63 | 65 | 67 | 68 | 70 |
| UQE 3500 | $14.6 \times \mathrm{C} 08$ | 107 | 7.5 | 57 | 59 | 62 | 63 | 64 |
| UTE 2240 | $3 \times \mathrm{C} 03$ | 71 | 1 | 53 | 55 | 58 | 60 | 61 |
| UTE 2240 | $3 \times \mathrm{C} 03$ | 71 | 7.5 | 48 | 50 | 53 | 55 | 56 |
| UDD 450 | $1 \times$ C05d | $\begin{gathered} 52 / 2= \\ 26 \\ \hline \end{gathered}$ | 1 | 61 | 60 | 61 | 61 | 62 |
| UDD 450 | $1 \times$ C05d | $\begin{gathered} 52 / 2= \\ 26 \\ \hline \end{gathered}$ | 7.5 | 55 | 54 | 55 | 56 | 57 |
| CPA 4000 | $2 \times \mathrm{C} 09 \mathrm{r}$ | $\begin{gathered} 159 / 3= \\ 53 \end{gathered}$ | 1 | 53 | 57 | 60 | 62 | 63 |
| CPA 4000 | $2 \times \mathrm{C} 09 \mathrm{r}$ | $\begin{gathered} 159 / 3= \\ 53 \\ \hline \end{gathered}$ | 7.5 | 47 | 51 | 54 | 56 | 57 |
| LOC5600/2600 | $1 \times \mathrm{C} 09 \mathrm{~m}$ | 19 | 1 | 51 | 53 | 56 | 58 | 60 |
| LOC5600/2600 | $1 \times \mathrm{C} 09 \mathrm{~m}$ | 19 | 7.5 | 45 | 47 | 51 | 52 | 54 |
| LOC1930/1960 | $1 \times \mathrm{C} 05 \mathrm{~d}$ | 20 | 1 | 61 | 60 | 61 | 61 | 62 |
| LOC1930/1960 | $1 \times \mathrm{C} 05 \mathrm{~d}$ | 20 | 7.5 | 55 | 54 | 55 | 56 | 57 |

Table 8: $L_{\text {AFmax }}$ values (roads)

| Vehicle | Distance to the road [m] | $L_{\text {AFmax }}$ values from $L_{\text {Aeq }}$ values of Table 5 [equation (4)] [dB(A)] |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $30 \mathrm{~km} / \mathrm{h}$ | $50 \mathrm{~km} / \mathrm{h}$ | Speed 80 km/h | $100 \mathrm{~km} / \mathrm{h}$ | $120 \mathrm{~km} / \mathrm{h}$ |
|  | NMPB'96 |  |  |  |  |  |
| Light | 1 | 85 | 880 | 94 | 98 | 100 |
| Light | 7.5 | 69 | 72 | 78 | 81 | 84 |
| Trucks | 1 | 101 | 100 | 102 | 106 | 107 |
| Trucks | 7.5 | 84 | 84 | 87 | 90 | 91 |
|  | CNOSSOS |  |  |  |  |  |
| Light | 1 | 80 | 85 | 91 | 95 | 98 |
| Light | 7.5 | 65 | 70 | 76 | 80 | 83 |
| Trucks (Cat.2) | 1 | 89 | 91 | 94 | 97 | 100 |
| Trucks (Cat.2) | 7.5 | 73 | 76 | 80 | 82 | 84 |
| Trucks (Cat.3) | 1 | 92 | 94 | 97 | 100 | 102 |
| Trucks (Cat.3) | 7.5 | 76 | 79 | 82 | 85 | 87 |

Table 9: $L_{\text {AFmax }}$ values for Portuguese Trains

| Train | Relation <br> to SRMI <br> Category | $\begin{aligned} & \text { Length } \\ & {[\mathrm{m}]} \end{aligned}$ | Distance to the railway [m] | $L_{A F m a x}$ values from $L_{A e q}$ values of Table 7 [equation (6)] [dB(A)] |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Speed [ $\mathrm{km} / \mathrm{h}$ ] |  |  |  |  |
|  |  |  |  | 30 | 50 | 80 | 100 | 120 |
| SRMII - Portuguese Trains |  |  |  |  |  |  |  |  |
| UQE 3150/3250 | $4.6 \times \mathrm{C} 02$ | 79 | 1 | 87 | 91 | 95 | 98 | 102 |
| UQE 3150/3250 | $4.6 \times \mathrm{C} 02$ | 79 | 7.5 | 81 | 85 | 90 | 93 | 96 |
| $\begin{gathered} \text { UQE 2X00+ } \\ \text { UQE2X00 } \end{gathered}$ | $25 \times \mathrm{C} 02$ | 192 | 1 | 90 | 94 | 99 | 102 | 105 |
| $\begin{aligned} & \text { UQE 2X00+ } \\ & \text { UQE2X00 } \end{aligned}$ | $25 \times \mathrm{C} 02$ | 192 | 7.5 | 85 | 89 | 93 | 96 | 100 |
| UQE 3500 | $14.6 \times \mathrm{C} 08$ | 107 | 1 | 87 | 92 | 95 | 97 | 100 |
| UQE 3500 | $14.6 \times \mathrm{C} 08$ | 107 | 7.5 | 81 | 85 | 90 | 92 | 94 |
| UTE 2240 | $3 \times \mathrm{C} 03$ | 71 | 1 | 79 | 83 | 88 | 91 | 93 |
| UTE 2240 | $3 \times \mathrm{C} 03$ | 71 | 7.5 | 74 | 78 | 82 | 85 | 88 |
| UDD 450 | $1 \times$ C05d | $\begin{gathered} 52 / 2= \\ 26 \\ \hline \end{gathered}$ | 1 | 91 | 93 | 95 | 96 | 98 |
| UDD 450 | $1 \times \mathrm{C} 05 \mathrm{~d}$ | $\begin{gathered} 52 / 2= \\ 26 \end{gathered}$ | 7.5 | 84 | 85 | 88 | 90 | 92 |
| CPA 4000 | $2 \times \mathrm{C} 09 \mathrm{r}$ | $\begin{gathered} 159 / 3= \\ 53 \end{gathered}$ | 1 | 80 | 87 | 91 | 94 | 96 |
| CPA 4000 | $2 \times \mathrm{C} 09 \mathrm{r}$ | $\begin{gathered} 159 / 3= \\ 53 \end{gathered}$ | 7.5 | 74 | 80 | 84 | 87 | 90 |
| LOC5600/2600 | $1 \times \mathrm{C} 09 \mathrm{~m}$ | 19 | 1 | 83 | 87 | 91 | 94 | 98 |
| LOC5600/2600 | $1 \times \mathrm{C} 09 \mathrm{~m}$ | 19 | 7.5 | 75 | 79 | 84 | 86 | 90 |
| LOC1930/1960 | $1 \times \mathrm{C} 05 \mathrm{~d}$ | 20 | 1 | 92 | 94 | 96 | 97 | 99 |
| LOC1930/1960 | $1 \times \mathrm{C} 05 \mathrm{~d}$ | 20 | 7.5 | 84 | 86 | 88 | 90 | 92 |

## 3. SOME PRATICAL RESULTS

To have an idea of real values, to check the theoretically values presented in Table 8 and Table 9, we can appeal to values measured in reality.

For roads, there are some results related with the Statistical Pass-by Measurements, at a distance of 7.5 m to the road. For example, the refence [7] shows, on his Fig.1, $L_{\text {AFmax }}$ for Cars at $80 \mathrm{~km} / \mathrm{h}$, from about $77 \mathrm{~dB}(\mathrm{~A})$ to $86 \mathrm{~dB}(\mathrm{~A})$, depending on the road surface. For trucks between about $87 \mathrm{~dB}(\mathrm{~A})$ to $94 \mathrm{~dB}(\mathrm{~A})$.

So, the values in Table 8, at 7.5 m , for $80 \mathrm{~km} / \mathrm{h}$, between $76 \mathrm{~dB}(\mathrm{~A})$ and $78 \mathrm{~dB}(\mathrm{~A})$, for cars, and between $80 \mathrm{~dB}(\mathrm{~A})$ and $87 \mathrm{~dB}(\mathrm{~A})$, for trucks, are similar to the reality values of reference [7].

We can compare also with the legal limits of the reference [8]. The legal limits are not exactly $L_{\text {AFmax }}$ at 7.5 m from the road at $50 \mathrm{~km} / \mathrm{h}$, but can be compared, safely, like that (because the vehicle is tested accelerating). So, we have, in Annex III of refence [8], for 2016 and for "Vehicles used for the carriage of passengers", values between $72 \mathrm{~dB}(\mathrm{~A})$ and $80 \mathrm{~dB}(\mathrm{~A})$, and for "Vehicles used for the carriage of goods", values between $72 \mathrm{~dB}(\mathrm{~A})$ and $82 \mathrm{~dB}(\mathrm{~A})$. In Table 8, at 7.5 m distance and $50 \mathrm{~km} / \mathrm{h}$, we have, for Light vehicles, values between $70 \mathrm{~dB}(\mathrm{~A})$ and $72 \mathrm{~dB}(\mathrm{~A})$, and for trucks between $76 \mathrm{~dB}(\mathrm{~A})$ and $84 \mathrm{~dB}(\mathrm{~A})$, which are very similar values with the legal limits.

For railways, in the reference [9], at point 1 (about 7.5 m from the railways), we have about $95 \mathrm{~dB}(\mathrm{~A})$ for $L_{A F m a x}$, for UDD circulating about $80 \mathrm{~km} / \mathrm{h}$, and about $85 \mathrm{~dB}(\mathrm{~A})$ for $L_{A F m a x}$, for UTE circulating about $70 \mathrm{~km} / \mathrm{h}$, what are values similar but higher than the values calculate and presented in Table 9.

More information must be obtained for the $L_{\text {Aeq }}$ and $L_{\text {AFmax }}$ of trains. Must be highlighted that some $L_{\text {Aeq }}$ values, during train pass-by, obtained on the reference [9], do not full feel the requirements of the reference [10].

## 4. NOISE MAPS

A typical software/method divides a road or a railway in small parts, each with some sound power level, in a way that, for the receiver points, the global $L_{\text {Aeq }}$ values is the energetic sum of the contribution of each small part.

For example, the software Cadna A [11], permit the calculation of $L_{A F m a x}$, for "industrial" sources (point, linear or area sources) if we know the difference between the $L_{\text {Aeq }}$ of each small part and $L_{A F m a x}$.

So, a way for the calculation of $L_{\text {AFmax }}$ Noise Maps, for roads and railways, is to divide the road or the railway in small parts (for example 1 m each; "Break into pieces" tool of the software), and calculate the $L_{\text {Aeq }}$ at 1 m distance, for just one of the small parts, and convert this part to a line source and adjust the sound power level of this line source to give the same $L_{\text {Aeq }}$ value on the receiver 1 m distance. We must create a line source spectrum accordingly with the spectrum of the pass-by we are considering.

Knowing the $L_{A F m a x}$ expected at this point (on the example 1m distance; so the values of Table 8 and Table 9 can be used, or others similar), for a certain pass-by of a certain vehicle, we calculate the difference between $L_{A F m a x}$ and $L_{\text {Aeq }}$. We must introduce this difference in the field "Res. PWL max" of the Line Source form (see Figure 1).


Figure 1: Example of $L_{\text {max }}$ table of Cadna $A$

In Figure 2 we can see the $L_{A e q}$ noise map of some road. In the Figure 3 we can see de $L_{\text {AFmax }}$ noise map of the same road, using the methodology described. As we can see, for some distances - as expected and explained on chapter 2 - the $L_{\text {Aeq }}$ noise map give greater values than $L_{A F m a x}$. So, the in fact $L_{\text {AFmax }}$ global noise map must be the maximum values of the two maps.


Figure 2: Example of $L_{\text {Aeq }}$ Noise Map of a road

| 44 | 44 | 44 | 44 | 44 | 44 | 44 | 44 | 44 | 44 | 44 | 44 | 44 | 44 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 46 | 46 | 46 | 46 | 46 | 46 | 46 | 46 | 46 | 46 | 46 | 46 | 46 | 46 |
| 47 | 47 | 47 | 47 | 47 | 47 | 47 | 47 | 47 | 47 | 47 | 47 | 47 | 47 |
| 49 | 49 | 49 | 49 | 49 | 49 | 49 | 49 | 49 | 49 | 49 | 49 | 49 | 49 |
| 52 | 52 | 52 | 52 | 52 | 52 | 52 | 52 | 52 | 52 | 52 | 52 | 52 | 52 |
| 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 |
| 58 | 58 | 58 | 58 | 58 | 58 | 58 | 58 | 58 | 58 | 58 | 58 | 58 | 58 |
| 62 | 62 | 62 | 62 | 62 | 62 | 62 | 62 | 62 | 62 | 62 | 62 | 62 | 62 |
| 68 | 68 | 68 | 68 | 68 | 68 | 68 | 68 | 68 | 68 | 68 | 68 | 68 | 68 |
| 78 | 78 | 78 | 78 | 78 | 78 | 78 | 78 | 78 | 78 | 78 | 78 | 78 | 78 |

Figure 2: Example of the $L_{A F m a x}$ Noise Map of the same road

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[^0]:    ${ }^{1}$ vitor.schiu@gmail.com
    ${ }^{2}$ aguileira.schiu@gmail.com

